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APPLICATIONS OF PARTIAL DIFFERENTIAL APPROXIMANTS:  
TEST FUNCTIONS AND DIMENSIONAL CROSSOVER IN THE  
ISING MODEL

by

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"APPLICATIONS OF PARTIAL DIFFERENTIAL APPROXIMANTS:  
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## ABSTRACT

The method of partial differential approximants (PDA) has been introduced for approximating functions of two or more variables given a finite number of coefficients of their power series. It is supposed to be effective close to the multicritical points, where the thermodynamic functions are expected to behave according to the scaling hypothesis. In order to assess the performance of the method, we have undertaken the construction of PDA's for several test functions of two variables. For some simple functions, which are represented exactly by PDA's and which exhibit an analog of a multicritical point, the numerical estimates yielded very good results even at lower orders. For other functions the estimates tended to improve as we increased the order of the approximants. For the best PDA's we constructed flow diagrams and estimated the scaling functions. Also, we have analyzed the dimensional crossover (from  $d=3$  to  $d=2$ ) of the spin  $-1/2$  axial anisotropic Ising model on the fcc lattice. We considered series expansions for the direct susceptibility and also for the sum of the direct and the staggered susceptibilities. In general, our estimates agree with the scaling predictions.

## I. INTRODUCTION

The usefulness of the Padé method for approximating functions of one variable given a finite number of coefficients of their power series is appreciated widely. In the theory of critical phenomena, for instance, the so-called d-log Padé approximants have been very practical for providing estimates of the critical parameters of thermodynamic model functions (Hunter and Baker 1973, Baker and Hunter 1973). These successes have stimulated some recent proposals to generalize the Padé method for approximating functions of two or more variables (Chisholm 1973, Roberts et al. 1975). The present publication refers to a proposal by Fisher (1977a, 1977b), which seems particularly suited for analyzing the scaling behavior of thermodynamic model functions in the neighborhood of their multicritical points.

In the conventional d-log Padé method (Baker 1975) the logarithmic derivative of a function  $f(x)$  is approximated as

$$\frac{d}{dx} \ln f(x) \approx \frac{P_L(x)}{Q_M(x)} = \frac{d}{dx} \ln F_{LM}(x) \quad (1.1)$$

where  $P_L(x)$  and  $Q_M(x)$  are polynomials of degrees  $L$  and  $M$  respectively. These rational approximants may represent well branch point singularities of the form

$$f(x) \approx A(x_c - x)^{-\gamma} \quad \text{for} \quad x \rightarrow x_c^-, \quad (1.2)$$

where  $\gamma$  is a nonintegral exponent. One should recall at this point that the approximants  $F_{LM}(x)$  may also be regarded as the solutions of the differential equation

$$P_L(x) F_{LM}(x) = Q_M(x) \frac{d}{dx} F_{LM}(x) \quad (1.3)$$

The coefficients  $p_\ell$  and  $q_m$  ( $\ell = 0, 1, \dots, L$ ;  $m = 0, 1, \dots, M$ ) of the polynomials  $P_L$  and  $Q_M$  in powers of  $x$  are then chosen so that the power series solution of Eq. (1.3) agrees with the expansion of  $f(x)$  to optimal order. In the critical region we have

$$Q_M(x) \approx Q'_C(x - x_C) \quad (1.4a)$$

and

$$P(x_C) = P_C = -\gamma Q'_C, \quad (1.4b)$$

which provide estimates of  $x_C$  and  $\gamma$ .

Let us consider a function of two variables  $x$  and  $y$ , given by the series expansion

$$f(x, y) = \sum_{k, k'=0} f_{k, k'} x^k y^{k'}, \quad (1.5)$$

where the indices  $k$  and  $k'$  belong to some set of integers  $\mathbb{K}$ . In analogy with Eq. (1.3), Fisher (1977a, 1977b) proposed a novel class of approximants for these functions,  $F_{LMN}(x, y)$ , defined as the solutions of the partial differential equation

$$P_L(x,y)F(x,y) = Q_M(x,y) \frac{\partial F(x,y)}{\partial x} + R_N(x,y) \frac{\partial F(x,y)}{\partial y} \quad (1.6)$$

subjected to suitable boundary conditions. The polynomials  $P_L$ ,  $Q_M$  and  $R_N$  are chosen so that the series solution for  $F(x,y)$  in powers of  $x$  and  $y$  agrees with the known expansion (1.5) as far as possible. This simply leads to a set of simultaneous linear equations which may be solved by standard numerical methods.

As we stated above, these "partial differential approximants" (which will be called PDA) are particularly effective when  $f(x,y)$  displays a singular behavior according to the scaling hypothesis of the theory of critical phenomena, that is, for

$$f(x,y) \approx |\Delta x|^{-\gamma} Z\left(\frac{\Delta y}{|\Delta x|^\phi}\right), \quad (1.7)$$

as  $\Delta x \equiv x - x_c \rightarrow 0$  and  $\Delta y \equiv y - y_c \rightarrow 0$ , where  $\gamma$  and  $\phi$  are two exponents, in general nonintegral, while  $Z(z)$  is a "scaling function" of a single variable  $z$ . In this case, it is easy to see that the multicritical point will be estimated by

$$Q_M(x_c, y_c) = R_N(x_c, y_c) = 0 \quad (1.8)$$

while the rate of variation of  $R_N$  and  $Q_M$  at the multicritical point, normalized by  $P_c = P_L(x_c, y_c)$ , will give estimates for the exponents  $\gamma$  and  $\phi$ .

To these days, except for some exploratory

trials, partial differential approximants have been tested only in the problem of the anisotropic exchange crossover in three-dimensional classical ferromagnets (Fisher and Kerr 1977). As far as we know, there have been no applications either to other physical problems of interest or to some model examples. The main point of our paper is thus to contribute for assessing the potentialities of the method by investigating numerically some classes of test functions, and also the dimensional crossover in the Ising model. We believe that our tests will reveal the advantages and some drawbacks (slow convergence, the need for longer series) of these partial differential approximants.

The layout of our paper is as follows. In Sec. II we consider a more general scaling form, where the scaling axes are not parallel to the cartesian axes, and introduce the method of characteristics for obtaining the numerical solutions of the partial differential equation (1.6). Also, we discuss the criteria for the stability of these solutions near the multicritical points. In Sec. III we study several model functions, some of which can be represented exactly by PDA's. We obtain the multicritical parameters, some flow diagrams, and try to compare the performance of different orders of PDA's. Sec. IV is about the analysis of the dimensional crossover, between dimensions  $d = 3$  and  $d=2$ , of the Ising model with lattice anisotropy. In particular, we use the PDA's for estimating the shape of the phase boundaries in the temperature-anisotropy phase diagram. Finally, a summary is presented in Sec. V.

## II. FURTHER DESCRIPTION OF THE METHOD

In general, the scaling axes are not parallel to the cartesian  $x, y$  axes. We thus have the scaling form

$$f(x, y) \approx |\Delta\tilde{x}|^{-\gamma} z\left(\frac{\Delta\tilde{y}}{|\Delta\tilde{x}|\phi}\right), \quad (2.1)$$

where

$$\Delta\tilde{x} = \Delta x - \frac{1}{e_2} \Delta y, \quad (2.2)$$

and

$$\Delta\tilde{y} = \Delta y - e_1 \Delta x. \quad (2.3)$$

The parameters  $e_1$  and  $e_2$  represent the slopes of the optimal scaling axes in the cartesian coordinate system specified by  $x$  and  $y$ .

The scaling form of Eq. (2.1) obeys the partial differential equation

$$\begin{aligned} (\Delta\tilde{x} + \frac{\phi}{e_2} \Delta\tilde{y}) \frac{\partial f}{\partial \Delta\tilde{x}} + (e_1 \Delta\tilde{x} + \phi \Delta\tilde{y}) \frac{\partial f}{\partial \Delta\tilde{y}} = \\ = -\gamma \left(1 - \frac{e_1}{e_2}\right) f, \end{aligned} \quad (2.4)$$

which should be compared, in the vicinity of the multicritical point  $(x_c, y_c)$ , with the defining differential equation (1.6)



of the PDA's. If the polynomials  $P_L$ ,  $Q_M$  and  $R_N$  in leading order close to the multicritical point are given by

$$P_L(x,y) \approx P_C, \quad (2.5)$$

$$Q_M(x,y) \approx Q_1 \Delta x + Q_2 \Delta y, \quad (2.6)$$

$$R_N(x,y) \approx R_1 \Delta x + R_2 \Delta y, \quad (2.7)$$

we may write the following expressions for the slopes of the scaling axes and the multicritical exponents,

$$e_{1,2} = \frac{1}{2} \frac{R_2 - R_1}{Q_2} \pm \frac{1}{2} \left[ \left( \frac{R_2 - R_1}{Q_2} \right)^2 + 4 \frac{R_1}{Q_2} \right]^{1/2}, \quad (2.8)$$

$$\gamma = \frac{P_C}{e_2 Q_2 - R_2}, \quad (2.9)$$

and

$$\phi = -1 - \gamma \frac{Q_1 + R_2}{P_C}. \quad (2.10)$$

Thus the estimate for the location of the multicritical point is given by  $Q_M(x_c, y_c) = R_N(x_c, y_c) = 0$ , while  $e_1, e_2, \gamma$  and  $\phi$ , are related to the rate of change of the polynomials  $Q_M$  and  $R_N$  at the estimated values  $(x_c, y_c)$  provided that  $P_L(x_c, y_c) \neq 0$ .

To estimate the actual values assumed by  $f(x,y)$ ,

Fisher (1977a) suggested the numerical solution of Eq. (1.6) via the method of characteristics. In the multicritical region, this corresponds to the evaluation of the scaling function  $Z(z)$ , which is often of interest in the theory of critical phenomena. Let us consider a time-like variable  $t$  such that

$$x = x(t) \quad , \quad y = y(t) \quad , \quad (2.11)$$

and

$$\frac{dx}{dt} = Q_M(x,y) \quad , \quad \frac{dy}{dt} = R_N(x,y) \quad . \quad (2.12)$$

From Eq. (1.6) we have

$$P_L(x,y) f(x,y) = \frac{d}{dt} f(x,y) \quad , \quad (2.13)$$

and, therefore,

$$f[x(t),y(t)] - f[x(0),y(0)] = \exp \left\{ \int_0^t P_L[x(t'),y(t')] dt' \right\} \quad , \quad (2.14)$$

where it should be stressed that the integration is performed along the trajectories defined by Eq. (2.12). Given the polynomials  $Q_M(x,y)$  and  $R_N(x,y)$ , the problem is then reduced to the solution of the set of coupled ordinary differential equations (2.12).

In problems of physical interest it is often important to know the loci of the singularities of the functions

$f(x,y)$  (for instance, the shapes of the phase boundaries near the bicritical point of an antiferromagnet in the field-temperature phase diagram). From Eq. (2.14), since  $P_L(x,y)$  is a finite polynomial, there is a finite difference between the values assumed by the function  $f(x,y)$ , calculated at two points which lie on the same trajectory. Therefore, the critical lines, where  $f(x,y)$  is supposed to diverge, are flow-lines defined by Eqs. (2.12). It is enough to know one single point on these trajectories, besides the multicritical point, to be able to construct them numerically. An illuminating application of this procedure, which will become more transparent in the following sections, is presented in the paper of Fisher and Kerr (1977).

In the neighborhood of the estimated multicritical point  $(x_c, y_c)$ , Eqs. (2.12) may be written as the linearized forms

$$\frac{dx}{dt} = Q_1 \Delta x + Q_2 \Delta y \quad , \quad (2.15a)$$

and

$$\frac{dy}{dt} = R_1 \Delta x + R_2 \Delta y \quad , \quad (2.15b)$$

which have the general solution

$$\Delta x = C_1 \exp(\lambda_1 t) + C_2 \exp(\lambda_2 t) \quad , \quad (2.16a)$$

and

$$\Delta y = C_1 e^{\lambda_1 t} + C_2 e^{\lambda_2 t} \quad (2.16b)$$

where  $C_1$  and  $C_2$  are arbitrary constants. The particular solutions with  $C_1 = 0$  or  $C_2 = 0$  define the scaling axes, and the eigenvalues  $\lambda_1$  and  $\lambda_2$  are given by

$$\lambda_{1,2} = \frac{1}{2} (Q_1 + R_2) \pm \frac{1}{2} \left[ (Q_1 - R_2)^2 + 4Q_2 R_1 \right] = Q_2 e_{1,2} + Q_1 \quad (2.17)$$

A complete discussion about the stability of Eqs. (2.16), which will define the behavior of the flow-lines in the immediate vicinity of the estimated multicritical point, may be found, for example, in the book by Brand (1966). In the case where  $\lambda_1, \lambda_2 < 0$ , all flow-lines in the neighborhood of  $(x_c, y_c)$  converge onto this estimated multicritical point. Although it is desirable to have a stable multicritical point, this is not strictly necessary for performing numerical evaluations of the function  $f(x, y)$ . The estimated values of  $(x_c, y_c)$  may happen to be a saddle point (for  $\lambda_1 \lambda_2 < 0$ ) or even a star-like unstable node.

Another interesting feature of the flow diagrams is the following expression for the slope of the flow lines in the immediate vicinity of the estimated multicritical point,

$$\frac{dy}{dx} = \frac{C_1 \lambda_1 e^{\lambda_1 t} + C_2 \lambda_2 e^{\lambda_2 t}}{C_1 \lambda_1 e^{\lambda_1 t} + C_2 \lambda_2 e^{\lambda_2 t}} \quad (2.18)$$

For  $\lambda_1 < \lambda_2 < 0$ , unless  $C_2 = 0$ , the value of  $dy/dx$  tends to

the slope  $e_2$  of the scaling axis as  $t \rightarrow \infty$ . This will become apparent in the analysis of the model functions which are considered in the next section.

Finally, a relevant question concerns the magnitude of the region where the predictions of the linear approximation still work. This may be estimated by the standard techniques associated with the Liapunov functions (Brand 1966).

### III. NUMERICAL RESULTS WITH TEST FUNCTIONS

We applied the technique of partial differential approximants to obtain numerical estimates pertaining to the following model functions:

(i) functions with one line of singularities

$$F_a = (1 - 2x - y)^{-3/2} \quad (3.1)$$

$$F_b = (1 - 2x - y)^{-3/2} \exp(-y) \quad (3.2)$$

(ii) functions with two lines of singularities

$$F_c = (1 - x - \frac{1}{2}y)^{-3/2} (1 - 2x - \frac{1}{5}y)^{-1/2} \quad (3.3)$$

$$F_d = (1 - x - 2y)^{-5/2} (1 - 3x - y)^{-2} \ln(1 - 3x - y) \quad (3.4)$$

$$F_e = (1-x-\frac{1}{2}y)^{-3/2} (1-2x-\frac{1}{5}y)^{-1/2} + \exp(-x-2y) \cos(xy) \quad (3.5)$$

$$F_f = (1-x-2y)^{-5/2} (1-3x-y)^{-2} + \exp(-x-2y) \cos(xy) \quad (3.6)$$

Functions  $F_a$  to  $F_d$  are represented exactly by PDA's of lower orders (as remarked by Fisher (1977a), they belong to a general class of functions which may be represented exactly). Roberts et al. (1975) have analyzed similar functions by the techniques of Canterbury approximants. Also, these functions may be regarded as the natural extensions of the one-variables functions which had been analyzed by the Padé method and other techniques by Hunter and Baker (1973).

The singular parts of the test functions (3.3) to (3.6) obey the general scaling form of Eq. (2.1) with two options for the scaling function  $Z(z)$ . For example, in the case of functions  $F_c$  and  $F_e$ , one of the options is

$$\Delta\tilde{x} = 1 - x - \frac{1}{2}y, \quad (3.7a)$$

and

$$\Delta\tilde{y} = 1 - 2x - \frac{1}{5}y, \quad (3.7b)$$

which leads to

$$e_1 = -10, \quad e_2 = -2, \quad \gamma - \frac{1}{2}\phi = \frac{3}{2}, \quad \text{and} \quad Z(z) = z^{-1/2}.$$

In the other option  $\Delta\tilde{x}$  and  $\Delta\tilde{y}$  are interchanged, leading to

$$e_1 = -2, \quad e_2 = -10, \quad \gamma - \frac{3}{2}\phi = \frac{1}{2}, \quad \text{and} \quad z(z) = z^{-3/2}.$$

For these functions, unlike in the case of the real physical problems, it is not possible to determine  $\gamma$  and  $\phi$  independently. Also, it should be remarked that  $F_c$  may be represented exactly by a set of PDA's where  $P_L$  has a constant value and the polynomials  $Q_M$  and  $R_N$  are linear in the variables  $x$  and  $y$ .

Functions  $F_a$  to  $F_f$  were represented as the power series

$$F(x,y) = \sum_{k,k'=0} f_{k,k'} x^k y^{k'} \quad (3.8)$$

with the coefficients  $f_{k,k'}$  corresponding to a triangular array (that is, with  $k+k' \leq o_s$ , where the integer  $o_s$  gives the order of the series). Also, the polynomials  $P_L$ ,  $Q_M$ , and  $R_N$  are given by the triangular arrays,

$$P_L(x,y) = \sum_{l,l'=0} p_{l,l'} x^l y^{l'}, \quad (3.9)$$

$$Q_M(x,y) = \sum_{m,m'=0} q_{m,m'} x^m y^{m'}, \quad (3.10)$$

and

$$R_N(x,y) = \sum_{n,n'=0} r_{n,n'} x^n y^{n'} \quad (3.11)$$

where the integers  $L, M$  and  $N$ , are the number of terms of the polynomials  $P_L, Q_M$  and  $R_N$ , respectively, and  $l+l' \leq o_P$ ,  $m+m' \leq o_Q$ , and  $n+n' \leq o_R$ . As we are fixing  $L, M$  and  $N$ , instead of the order  $o_P, o_Q$ , and  $o_R$ , the polynomials  $P_L, Q_M$  and  $R_N$  may not be symmetric in terms of the variables  $x$  and  $y$ . For example, the polynomial  $P_L$ , with  $L=4$ , is written as

$$P_4(x,y) = p_{00} + p_{10}x + p_{01}y + p_{20}x^2 \quad (3.12)$$

If we make  $p_{00} = 1$ , the  $L+M+N-1$  remaining coefficients of the polynomials are determined by the set of linear equations which come from the substitution of the series expansion (3.8) into Eq. (1.6). Given a series of order  $o_S$ , we may construct approximants of order  $o_A$ , such that

$$o_A \leq o_S - 1 \quad (3.13)$$

where

$$L+M+N-1 = \frac{(o_A+1)(o_A+2)}{2} \equiv K(o_A) \quad (3.14)$$

The construction of all PDA's up to a certain order, in analogy with the standard Padé tables, is a rather formidable task even at not so high orders. Indeed, the number of approximants



of order  $o_A$  is given by

$$K[K(o_A)] = \frac{(o_A+1)^2(o_A+2)^2}{8} + \frac{3}{4}(o_A+1)(o_A+2) + 1 \quad (3.15)$$

This clearly imposes sharp limitations on the numerical calculations. Therefore, we have chosen 88 approximants, up to order 13, in a somewhat arbitrary fashion. As defined in Table I, we included diagonal and near-diagonal approximants ( $L \approx M \approx N$ ), as well as some off-diagonal ones.

It has been impossible to construct numerical approximants for  $F_a$ , even at the lowest orders, due to ill conditioned equations. With the exception of some off-diagonal approximants, the estimates for the critical points of  $F_b$  lie along the critical line, and tend to cluster around the intersection with the cartesian axes. For  $F_c$  and  $F_d$ , even at the lowest orders, we obtained nearly exact results for the multicritical points, the slopes of the scaling axes and the multicritical exponents. However, some off-diagonal approximants give estimates of the multicritical point which concentrate along one of the critical lines. For these functions the system of linear equations tends to become ill conditioned as we increase the order of the PDA's.

Due to the regular terms added to their singular parts, functions  $F_e$  and  $F_f$  are not represented exactly by finite partial differential approximants. For function  $F_f$  the singularities are stronger and closer to the origin than for  $F_e$ . So, it was not surprising to verify that  $F_f$  is

better represented than  $F_e$  with PDA's of lower orders. A sample of the estimates for the multicritical parameters of  $F_e$  and  $F_f$  is given in Tables II and III respectively. As a general pattern, the quality of the estimates improves as we increase the order of the approximants. Also, diagonal and near-diagonal approximants tend to produce better estimates than off-diagonal ones. Tables IV and V give ordered sequences of approximants according to the decreasing precision of their estimates. By the inspection of these sequences, it becomes apparent that there exists a correlation between the quality of different estimates: usually, a PDA which gives a good estimate of the location of the multicritical point, also happens to produce good estimates of the slopes of the scaling axes and of the multicritical exponents.

After obtaining the estimates of the multicritical parameters, we used the method of characteristics for solving numerically the differential equation (1.6). It turns out that most approximants for  $F_c$  to  $F_f$ , despite yielding good estimates for the multicritical parameters, display a saddle point unstable multicritical point in their flow-diagrams. As a matter of fact, no correlations were apparent between the quality of the estimates and the stability of the multicritical point.

In Fig. 1 we show the flow-diagram corresponding to the approximant number 1 for  $F_c$  ( $L=1$ ,  $M=N=3$ ). Within the numerical precision, this particular approximant belongs to the set of PDA's which represent  $F_c$  exactly. Since the polynomials  $Q_M$  and  $R_N$  are linear in  $x$  and  $y$ , the

system of coupled ordinary differential equations (2.14) is already linearized, and we can find solutions that hold in all regions of the  $x, y$  plane. In particular, since the estimated multicritical point is stable, every flow-line, no matter its starting point, converges onto  $(x_c, y_c)$ . The characterization of the critical lines as flow-lines, and the asymptotic alignment of the flow-lines with the scaling axis of slope  $e_1 = -10$  (associated with the smallest value of  $|\lambda|$ ), are also apparent from Fig. 1. Estimates of  $F_c$  along some flow-lines were obtained by the numerical evaluation of Eq. (2.14). Of course, in the case of this particular PDA, the defining equation (1.6) can be solved exactly, so that our numerical calculations could be controlled against the corresponding exact results. For example, in Fig. 1, if we start at the beginning of the flow-lines with the exact value of  $F_c$ , after a time interval of about 3 units, which already leads to the vicinity of the multicritical point, the usual error of our computer program amounts to about 0.3%.

The flow-lines corresponding to the approximant number 73 for  $F_f$  ( $L = 35$ ,  $M = 34$ ,  $N = 37$ ) are shown in Fig. 2. This PDA exhibits a stable multicritical point with the same features of the previous one. The asymptotic alignment of the flow-lines with the scaling axis corresponding to  $e_1 = -3$  is more striking in this case. This is due to the larger value of the difference  $|\lambda_1 - \lambda_2|$ . The estimates for  $F_f$  have a typical error of about 1% after an interval of 3 time units. In these numerical calculations, we used a Runge-Kutta method of fourth order for obtaining the flow diagrams,

and a Simpson procedure for performing the integrations, without worrying about the precision of the results.

#### IV. DIMENSIONAL CROSSOVER IN THE ISING MODEL

An Ising model with axial anisotropy may be defined by the Hamiltonian

$$\mathcal{H} = -J \sum_{(i,j)}^{(x,y)} s_i s_j - RJ \sum_{(i,j)}^{(z)} s_i s_j - H \sum_i s_i - H_{st} \sum_i (-1)^{\eta_i} s_i \quad (4.1)$$

where  $s_i = \pm 1$ , the first sum is over nearest neighbor pairs in the  $x$ - $y$  planes, and the second sum is over nearest neighbor pairs whose relative displacement vector has a  $z$  component.  $H$  stands for the applied magnetic field, and  $H_{st}$  for a staggered magnetic field which acts oppositely on adjacent planes of constant  $z$  (the parameter  $\eta_i$  is 0 or 1 depending on whether  $s_i$  belongs to an even or to an odd  $x$ - $y$  plane). In this work we consider  $J > 0$  only, so that for  $R > 0$  the system orders ferromagnetically, while it exhibits metamagnetic behavior for  $R < 0$ . The special value  $R = 0$  corresponds to a set of uncoupled two-dimensional ferromagnetic Ising models. Therefore, according to the ideas of smoothness and universality, an abrupt change in the values of the critical exponents is expected to occur at  $R = 0$ . The method of partial differential approximants is quite suitable for studying this dimensional crossover between  $d = 3$  and  $d = 2$ .

Harbus et al (1973) studied the four-dimensional phase diagram, in the  $T-H-H_{st}-R$  space, and some thermodynamic properties of this model. In particular, they identified a tetracritical point, where two ferromagnetic and two anti-ferromagnetic phases become identical, at  $R=H=H_{st}=0$  and  $T$  is equal to the critical temperature  $T_c$  of the two-dimensional Ising model. Using the symmetry properties of the model Hamiltonian (4.1), one can easily establish the following relation

$$\mathcal{Z}(T, R, H = H_0, H_{st} = 0) = \mathcal{Z}(T, -R, H = 0, H_{st} = H_0), \quad (4.2)$$

where  $\mathcal{Z}$  is the canonical partition function. From Eq. (4.2) we may write

$$\chi(T, R, H = H_0, H_{st} = 0) = \chi_{st}(T, -R, H = 0, H_{st} = H_0), \quad (4.3)$$

where  $\chi$  and  $\chi_{st}$  are the direct and the staggered susceptibilities of the model system. Thus, in zero fields, Harbus and Stanley (1973) formulate the scaling hypotheses

$$\chi(\tau, R) \approx |\tau|^{-\gamma} Z\left(\frac{R}{|\tau|^\phi}\right) \quad (4.4)$$

for  $R > 0$ , and

$$\chi_{st}(\tau, R) \approx |\tau|^{-\gamma} Z\left(-\frac{R}{|\tau|^\phi}\right) \quad (4.5)$$

for  $R < 0$ , with  $\tau \equiv (T - T_c)/T_c$ , and  $\gamma = \phi = 1.75$ . The critical

lines which are incident on the tetracritical point are associated with the singularity of the scaling function at  $z_t$ . They are described, therefore, in the vicinity of this multicritical point, by the symmetrical curves

$$\phi = \pm \frac{R}{z_t} \quad (4.6)$$

Although the one-variable series analyses, which were performed by Krasnow et al (1973), seem to support the scaling prediction, we decided to construct PDA's for the two-variable series expansions obtained by Harbus and Stanley (1973). Besides checking the previous analyses, the PDA's are expected to produce numerical results for the crossover exponent  $\phi$  and the shapes of the phase boundaries near the tetracritical point.

We considered a triangular series of order 10 for the reduced susceptibility,  $\bar{\chi} = \frac{kT\chi}{N}$ , of the model system defined by the Hamiltonian (4.1) on an fcc lattice. Using the variables

$$x \equiv \tanh \frac{J}{kT} \quad \text{and} \quad y \equiv \tanh \frac{RJ}{kT} \quad (4.7)$$

we constructed 61 approximants of orders 7, 8 and 9. This is the complete set of PDA's, up to these orders, with  $L \geq 1$  and  $M = N \geq 3$ . In Fig. 3 the estimates for the location of the tetracritical point are presented. The exactly known tetracritical point,

$$x_t = \sqrt{2} - 1 \quad , \quad y_t = 0 \quad ,$$

is also indicated in this figure, as well as intervals of  $\pm 1\%$  and  $\pm 10\%$  of  $x_t$ . We do not note any alignment of the estimates along the critical line, although they clearly tend to be situated on the half-plane  $y > 0$  (which indicates the influence of the ferromagnetic critical line). In Fig. 4 we see estimates for  $\gamma$  as a function of estimates for  $x_t$ . The values  $\gamma = 1.25$  and  $\gamma = 1.75$  are indicated. The estimates for  $\gamma$  are plotted against the estimates for  $y_t$  in Fig. 5. In Fig. 6, estimates for  $\phi$  are plotted against estimates for  $\gamma$ . The straight line  $\gamma = \phi$  was drawn in order to test the agreement of the results with the scaling prediction  $\gamma = \phi = 1.75$ . Some correlations are observed in this figure, but they do not allow any conclusions. Finally, one may observe that the estimates for  $e_1$  and  $e_2$  vary in a rather large interval. However, all estimates are such that  $|e_1| < 1$  and  $|e_2| > 1$ . In particular, those approximants whose estimates for the tetracritical point are close to the exact known location yield values for  $e_1$  and  $e_2$  such that  $|e_1| \ll 1$  and  $|e_2| \gg 1$ . This seems to indicate that the original  $x$  and  $y$  axes are indeed the proper scaling axes.

We believe that the nature of the tetracritical point as a terminal point of the ferromagnetic line may be one of the reasons for the rather poor performance of the approximants in this problem. In order to work with a quantity which takes into account the symmetry of the model, we defined the average reduced susceptibility,

$$\bar{\chi}_m = \frac{1}{2} (\bar{\chi} + \bar{\chi}_{st}) \quad (4.8)$$

which diverges at the critical line for both  $R > 0$  and  $R < 0$ . From (4.3), the series expansion for  $\bar{\chi}_m$  may be obtained trivially from the series for  $\bar{\chi}$  by a mere suppression of all odd terms in  $y$ . Thus, from the defining equations of the PDA's it is possible to have  $P_L$  and  $Q_M$  even in  $y$  and  $R_N$  odd. This really happens numerically, and leads to the fixed value  $y_t = 0$  in the estimates for the tetracritical point. In the approximants for  $\bar{\chi}_m$  we noted a large number of cases where ill-conditioned equations were obtained. It was impossible to construct any approximant of order 8, but there were 55 approximants of order 9 which, despite being off-diagonal, displayed well conditioned linear equations. Fig. 7 shows estimates for  $\gamma$  as functions of estimates for  $x_t$ . The marked point  $x_t = \sqrt{2} - 1$ ,  $\gamma = 1.75$  indicates that the results are really consistent with the expected values. The apparent dispersion of the estimates and the linear correlation they reveal is known from d-log Padé results for one variable series. Fig. 8, where we plotted estimates of  $\phi$  versus estimates of  $x_t$ , shows a similar behavior. Finally, Fig. 9, which displays estimates of  $\gamma$  versus estimates of  $\phi$ , seems to indicate very strongly that we really have  $\gamma = \phi = 1.75$  for this model. It is to be emphasized that in this case the values  $e_1 = 0$  and  $e_2 \rightarrow \infty$  are fixed by symmetry.

We also constructed flow diagrams for some of the best approximants to the original series for  $\bar{\chi}$  and for



$\bar{\chi}_m$ . It is remarkable that the best approximants exhibit locally stable tetracritical point estimates. The starting points of the flow-lines were located on a circle of radius  $r=0.32862$  and centered at  $(\sqrt{2}-1, 0)$ , which contains the estimated critical point  $(x_c=0.10174, y_c=0.10174)$  of the isotropic Ising model on an fcc lattice (Sykes (1972)).

Fig. 10 shows the flow-diagram for an approximant of order 9 ( $L=25, M=N=15$ ) for the series expansion of  $\bar{\chi}$ . This approximant gives the estimates

$$x_t = 0.411873 ,$$

$$y_t = -3.56741 \times 10^{-5}$$

and

$$e_1 = -1.415158 \times 10^{-2} , \quad e_2 = 2.34177 ,$$

$$\gamma = 1.87897 , \quad \phi = 1.79030 .$$

It is apparent the alignment of most flow-lines with the scaling axis with slope  $e_1$ . The marked flow-line corresponds to the estimated critical boundary. A log-log plot of  $x-x_t$  versus  $y-y_t$  for this particular line provides another estimate for  $\phi$ . The points are linearly correlated, even in regions not so close to the tetracritical point. If one estimates the slope grafically, it is possible to obtain  $\phi = 1.6 \pm 0.2$ .

Finally, Fig. 11 shows the flow-diagram for an

approximant of order 9 ( $L = 21$ ,  $M = 30$ ,  $N = 5$ ) for the series expansion of  $\bar{\chi}_m$ . The estimated tetracritical parameters are

$$x_t = 0.4146114 ,$$

$$\gamma = 1.7659 ,$$

$$\phi = 1.7840 ,$$

while

$$y_t = 0 , \quad e_1 = 0 , \quad e_2 \rightarrow \infty ,$$

are fixed by the biased symmetry requirements. Due to the parity of the polynomials, the flow-diagram is symmetric, so only the half-plane  $y > 0$  is displayed. The same features observed in the former flow-diagram are visible here, but a log-log plot of the estimated critical line produces the result  $\phi = 1.75 \pm 0.02$ , which manifests the better quality of these estimates.

## V. SUMMARY

We used finite double-variable power series of some test functions and thermodynamic model functions to assess the performance of the partial differential approximants for estimating multicritical parameters and phase boundaries.

The test functions were chosen so that their singular parts simulate the kind of multicritical behavior which is expected to occur in physical situations. Some test

functions could be represented exactly by PDA's. In this case we obtained excellent numerical results with approximants of lower orders. The accuracy of the estimates for the test functions which could not be represented exactly by approximants of finite order tended to improve as we increased the order of the approximants. This happened even in cases where approximants of relatively lower orders provided quite erratic estimates. Also, we used the method of characteristics to obtain numerical solutions for the defining differential equations of some approximants. It was possible to verify a strong correlation between the quality of the estimates for the multicritical parameters and the accuracy of these numerical solutions.

With the purpose of analyzing the crossover behavior between two and three dimensions, we constructed PDA's for the series expansion of the direct susceptibility of the axial anisotropic Ising model. The quality of the estimates improved considerably as we turned to the analysis of the more symmetric series expansion corresponding to the sum of the direct and the staggered susceptibilities. Besides using the PDA's for obtaining numerical estimates of the multicritical parameters, we also performed numerical solutions of the defining differential equations for some approximants. This procedure gives an estimate of the critical line in the anisotropy( $R$ )-temperature( $T$ ) plane and an additional estimate of the crossover exponent  $\phi$ . It is worth remarking that, despite the good overall agreement with the scaling predictions, the existent series expansions are a bit too short

for providing really excellent estimates by means of the PDA's.

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TABLE CAPTIONS

TABLE I - Specifications of the approximants to the power series of the test functions. The approximants were numbered from 1 to 88; L, M and N stand for the number of terms in the polynomials  $P_L$ ,  $Q_M$  and  $R_N$ , respectively.

TABLE II - Estimates for the "critical parameters" of the test function  $F_e = (1 - x - \frac{1}{2}y)^{-3/2} (1 - 2x - \frac{1}{5}y)^{-1/2} + \exp(-x - 2y) \cos xy$ , provided by a subset of the approximants defined in Table I.

TABLE III - Estimates for the "critical parameters" of the test function  $F_f = (1 - x - 2y)^{-5/2} (1 - 3x - y)^{-2} + \exp(-x - 2y) \cos xy$ , for the same subset of PDA's presented in Table II.

TABLE IV - Ordered sequences of PDA's to function  $F_e$ , according to the decreasing precision of their estimates. The parameters used in the ordering procedure are:  $\Delta_c$  - distance between the estimated and the exact "multicritical point";  $\Delta_1$  - distance between the estimated "multicritical point" and the straight line  $1 - x - \frac{1}{2}y = 0$ ;  $\Delta_2$  - distance between the estimated "multicritical point" and the straight line  $1 - 2x - \frac{1}{5}y = 0$ ;  $\Delta_{\text{exp}}$  - distance between the estimated exponents  $(\gamma, \phi)$  and the straight line  $\gamma - \frac{1}{2}\phi = \frac{3}{2}$  for the scaling option with  $e_1 \sim 10$  and  $e_2 \sim 2$ ;  $\Delta e_1$  - absolute difference between the exact and the estimated values for  $e_1$ ;

$\Delta e_2$  - absolute difference between the exact and the estimated values for  $e_2$ ;  $\Delta e$  - equals to

$$\sqrt{(\Delta e_1)^2 + (\Delta e_2)^2} .$$

TABLE V - Ordered sequences of PDA's to function  $F_f$ , according to the decreasing precision of their estimates. The parameters used in the ordering procedure are the same as defined in the caption of Table IV, with the exception of:  $\Delta_1$  - distance between the estimated multicritical point and the straight line  $1-x-2y=0$ ;  $\Delta_2$  - distance between the estimated multicritical point and the straight line  $1-3x-y=0$ ;  $\Delta_{\text{exp}}$  - distance between the estimated exponents  $(\gamma, \phi)$  and the straight line  $\gamma-2\phi = \frac{5}{2}$  for the scaling option with  $e_1 \sim -3$  and  $e_2 \sim -\frac{1}{2}$ .

## FIGURE CAPTIONS

FIG.1 - Flow diagram in the  $(x,y)$  plane of the PDA n<sup>o</sup> 1 ( $L=1$ ,  $M=N=3$ ) for the function  $F_c$ . The heavier lines indicate the trajectories which correspond to the scaling axes. The dots on the flow lines are spaced in unitary "time" intervals.

FIG.2 - Flow diagram in the  $(x,y)$  plane of the PDA n<sup>o</sup> 73 ( $L=35$ ,  $M=34$ ,  $N=37$ ) for the function  $F_d$ . The symbols have the same meaning as in Fig. 1.

FIG.3 - Estimates for the location of the tetracritical point  $(x_t, y_t)$  for the series expansion of the susceptibility of the axial anisotropic spin-1/2 Ising model on the fcc lattice. The crosses, open dots, and full dots indicate PDA's of orders 9, 8, and 7 respectively. Intervals of  $\pm 10\%$  and  $\pm 1\%$  about the exact value of  $x_t$  are also indicated.

FIG.4 - Estimates for the tetracritical exponent  $\gamma$  plotted against estimates for  $x_t$ . The symbols are the same as in Fig.3. The dashed lines indicate the values of the critical exponent  $\gamma$  for the two and the three-dimensional Ising model, and the exact value of  $x_t$  for the two-dimensional Ising model.

FIG.5 - Estimates for the tetracritical exponent  $\gamma$  plotted against estimates for  $y_t$ . The symbols have been defined in the captions of Figs. 3 and 4.



FIG.6 - Estimates for the tetracritical exponent  $\gamma$  plotted against estimates of the crossover exponent  $\phi$ . The scaling prediction  $\gamma = \phi = 1.75$  is also indicated in this figure.

FIG.7 - Estimates for the tetracritical exponent  $\gamma$  plotted against estimates for  $x_t$ . All crosses represent results from approximants of order 9 to the series expansion of the average susceptibility  $\left(\frac{1}{2} \chi + \frac{1}{2} \chi_{st}\right)$  of the axial anisotropic Ising model on the fcc lattice. The big cross indicates the exact location of  $x_t$  and the scaling prediction for  $\gamma$ .

FIG.8 - Estimates for the crossover exponent  $\phi$  plotted against estimates of the tetracritical parameter  $x_t$ . The order of the approximants as well as the series expansion which has been used and all the symbols of this figure are the same as in Fig.7.

FIG.9 - Estimates for the crossover exponent  $\phi$  plotted against estimates for the tetracritical exponent  $\gamma$ . We are using approximants of order 9 for the series expansion of the average susceptibility of the axial anisotropic Ising model. The scaling prediction  $\gamma = \phi = 1.75$  is indicated by the big cross.

FIG.10 - Flow diagram, in the  $(x = \tanh J/kT, y = \tanh RJ/kT)$  plane associated with a PDA of order 9, given by  $L = 26, M = N = 15$ , for the series expansion of the reduced direct susceptibility of the axial anisotropic

Ising model on the fcc lattice. The dot-dashed lines indicate the estimated scaling axes. The heavy line indicates the estimated phase boundary.

FIG.11 - Flow diagram, in the  $(x = \tanh J/kT, y = \tanh RJ/kT)$  plane, associated with a PDA of order 9, given by  $L = 21, M = 30, N = 5$ , for the series expansion of the reduced average susceptibility of the axial anisotropic Ising model on the fcc lattice. The scaling axes are fixed by symmetry. The heavy line indicates the estimated phase boundary.

I	L	M	N	I	L	M	N	I	L	M	N	I	L	M	N
1	1	3	3	23	23	22	22	45	3	26	50	67	15	74	3
2	4	6	6	24	22	23	22	46	59	10	10	68	36	35	35
3	2	5	15	25	22	22	23	47	10	59	10	69	35	36	35
4	2	10	10	26	25	21	21	48	10	10	59	70	35	35	36
5	7	5	25	27	21	25	21	49	66	7	6	71	37	34	35
6	7	15	15	28	21	21	25	50	30	31	31	72	34	35	37
7	7	25	5	29	37	15	15	51	31	30	31	73	35	34	37
8	4	21	21	30	49	15	3	52	31	31	30	74	35	37	34
9	6	5	35	31	15	3	49	53	29	31	32	75	34	36	36
10	6	20	20	32	3	49	15	54	31	29	32	76	36	34	36
11	6	35	5	33	3	32	32	55	32	29	31	77	36	36	34
12	16	15	15	34	15	26	26	56	32	31	29	78	45	31	30
13	36	5	5	35	27	26	26	57	29	32	31	79	45	30	31
14	6	5	45	36	26	27	26	58	31	32	29	80	28	39	39
15	6	15	35	37	26	26	27	59	28	32	32	81	30	30	38
16	6	25	25	38	23	28	28	60	20	36	36	82	38	34	34
17	6	35	15	39	37	21	21	61	36	28	28	83	50	28	28
18	6	45	5	40	21	37	21	62	10	41	41	84	3	52	51
19	14	21	21	41	21	21	37	63	45	23	24	85	3	51	52
20	18	4	34	42	3	38	38	64	45	24	23	86	10	21	75
21	18	19	19	43	67	6	6	65	3	15	74	87	21	75	10
22	18	34	4	44	3	50	26	66	74	3	15	88	21	10	75

TABLE I

I	$x_c$	$y_c$	$e_1$	$e_2$	$\gamma$	$\phi$
12	0.3186	2.318	10.66	-2.128	5.537	-7.091
15	0.4612	0.6485	-2.566	$-5.6 \times 10^{-2}$	0.5964	0.5928
23	0.4668	0.4075	-19.80	-0.7800	3.139	5.695
27	0.1893	$-4 \times 10^{-4}$	30.39	1.004	0.1857	2.164
30	0.5921	-0.9837	-10.08	-0.5056	-0.7342	-2.605
34	0.4547	0.3446	-6.248	0.9314	-0.3029	-0.9209
37	0.3913	1.413	-22.18	-2.002	-0.5770	-5.599
49	0.8315	-1.419	-1.286	1.082	-1.025	-2.038
50	0.3406	1.305	-5.917	-2.004	1.185	-0.5753
66	0.4570	0.7495	-18.78	-3.845	0.3050	-0.6100
68	0.3806	1.265	-12.08	-1.998	0.2370	-2.653
72	0.3735	1.256	-9.685	-1.995	-0.3188	-3.646
76	0.4268	1.244	17.86	-1.748	0.9843	-2.899
82	0.3739	1.248	-9.557	-1.995	$4.5 \times 10^{-2}$	-2.786
85	0.3742	1.224	-9.224	-2.026	-0.261	-3.229
87	0.4061	1.036	-16.14	-2.149	-0.3537	-2.350

TABLE II

I	$x_c$	$y_c$	$e_1$	$e_2$	$\gamma$	$\phi$
12	0.1884	0.4059	-2.950	-0.5044	0.4094	-1.104
15	0.2035	0.4457	-3.712	-0.4022	-1.273	-2.043
23	0.1989	0.3987	-2.966	-0.5030	-0.5720	-1.547
27	0.2000	0.4000	-3.001	-0.5003	-0.2923	-1.398
30	0.2353	0.3693	-4.141	-0.5071	0.9854	-0.3429
34	0.2000	0.3999	-3.001	-0.5003	$-6.67 \times 10^{-2}$	-1.217
37	0.2001	0.3999	-3.004	-0.5004	$6.53 \times 10^{-2}$	-1.216
49	$9.34 \times 10^{-2}$	0.6537	-2.662	-0.2878	-79.82	-1.525
50	0.2001	0.4001	-3.007	-0.4991	1.017	-0.7439
66	0.2635	0.3179	-4.307	-0.5884	-3.484	-0.9281
68	0.2000	0.4006	-3.020	-0.5000	-13.81	-8.160
72	0.2001	0.4004	-3.018	-0.4999	-11.03	-6.767
76	0.2001	0.4000	-3.002	-0.5000	-0.8118	-1.655
82	0.2021	0.3974	-1.467	$7.85 \times 10^{-2}$	4.583	1.066
85	0.2003	0.4008	-3.018	-0.4959	-0.1895	-1.344
87	0.2341	0.3296	-10.89	$-5.04 \times 10^{-2}$	4.621	1.526

TABLE III

ORDERED APPROXIMANTS ACCORDING TO INCREASING VALUES OF  $\Delta_c$

82	72	73	75	74	77	69	53	68	70	55	57	81	86	85	71	64	79	41
78	76	83	50	52	62	58	88	84	60	38	37	28	87	54	80	63	14	29
24	31	45	9	59	61	47	66	15	13	25	23	20	26	34	2	21	6	12
17	39	27	5	43	44	42	48	16	22	35	40	19	4	46	3	8	33	36
32	11	10	30	1	49	65	67	56	51	7	18							

INCREASING VALUES OF  $\Delta_1$

72	82	57	88	50	75	74	73	77	86	69	81	70	68	85	55	53	41	71
64	79	83	52	62	78	58	20	60	76	16	84	14	87	31	47	18	37	54
40	80	38	28	24	29	22	63	66	59	61	45	15	36	2	13	67	25	17
23	21	26	34	6	9	39	12	42	48	35	3	4	19	46	33	27	8	11
49	32	30	10	5	43	44	65	56	51	1	7							

INCREASING VALUES OF  $\Delta_2$

13	57	72	41	39	4	82	42	11	46	35	19	85	75	74	83	73	77	69
81	58	30	64	79	70	68	54	52	71	23	55	62	24	87	34	33	80	26
21	29	53	78	6	60	48	61	86	25	59	84	15	50	10	66	37	14	31
88	28	3	63	12	32	76	65	38	45	56	2	17	49	51	47	7	20	27
9	22	5	43	44	40	16	67	36	1	8	18							

INCREASING VALUES OF  $\Delta_{exp}$

72	58	20	50	86	52	74	65	70	82	68	73	69	77	57	75	81	53	71
85	55	45	79	31	28	83	41	60	47	62	78	14	84	54	87	37	46	66
30	80	38	33	24	8	48	59	29	15	23	61	32	34	9	42	6	19	26
39	22	4	1	5	16	17	25	43	44	88	49	63	3	35	27	11	76	36
13	40	56	2	12	51	10	21	7	67	18	64							

INCREASING VALUES OF  $\Delta_{e_1}$

30	12	76	46	72	33	39	19	41	42	82	24	57	51	85	13	35	54	56
21	73	64	74	75	81	4	86	52	77	71	55	69	79	70	7	53	68	48
10	60	58	29	80	27	6	11	26	34	84	78	61	83	50	32	28	62	59
38	63	8	87	2	40	15	18	47	36	49	66	22	67	65	23	1	5	16
17	25	43	44	88	37	14	3	31	45	20	9							

INCREASING VALUES OF  $\Delta_{e_2}$

64	70	68	37	50	72	82	62	73	74	69	55	77	60	53	81	71	85	75
79	83	57	52	86	41	24	78	28	87	84	58	80	38	29	31	20	54	48
35	65	32	45	8	6	42	39	61	33	23	13	47	46	30	2	4	19	3
66	40	15	59	26	67	18	1	5	16	17	25	43	44	88	22	9	34	49
36	11	63	14	56	51	12	76	10	27	7	21							

INCREASING VALUES OF  $\Delta_e$

72	41	82	24	57	85	54	35	42	39	73	64	33	74	75	81	30	46	13
86	52	19	77	71	55	69	79	70	53	68	4	48	60	58	29	80	6	84
78	83	50	61	26	28	62	32	34	59	11	38	8	87	2	40	15	47	18
63	66	65	36	67	49	22	23	1	5	16	17	25	43	44	88	37	56	51
12	3	76	14	10	27	31	45	7	21	20	9							

TABLE IV

ORDERED APPROXIMANTS ACCORDING TO INCREASING VALUES OF  $\Delta_c$

27	34	76	58	53	36	52	56	59	50	51	62	37	80	57	61	35	60	38
72	71	78	69	83	26	64	70	75	68	77	33	21	85	55	86	28	39	84
42	54	74	29	23	24	41	19	81	46	82	79	73	25	45	40	48	12	10
44	88	8	31	47	15	30	65	13	87	6	66	20	43	14	9	4	32	5
7	49	3	17	63	22	18	2	67	16	11	1							

INCREASING VALUES OF  $\Delta_1$

76	39	27	83	58	34	62	35	37	52	12	56	36	38	53	51	50	59	80
33	61	57	78	60	64	72	71	69	77	70	26	68	75	28	21	55	86	85
54	84	74	42	82	29	24	23	41	19	81	46	79	73	25	31	47	45	40
48	30	32	14	10	88	8	44	15	13	66	87	65	43	20	6	9	2	4
7	5	49	22	18	3	17	63	67	11	16	1							

INCREASING VALUES OF  $\Delta_2$

54	34	56	27	36	77	52	76	58	53	67	37	62	64	59	80	38	50	35
51	60	57	72	69	70	68	61	55	75	74	86	83	71	22	73	78	42	26
85	18	79	33	21	39	28	29	84	82	23	81	24	19	41	46	25	45	40
8	10	20	88	12	87	48	31	15	43	49	47	44	30	65	66	7	4	6
13	14	32	5	9	16	3	17	63	2	11	1							

INCREASING VALUES OF  $\Delta_{exp}$

52	53	51	69	60	56	77	58	62	85	76	80	36	37	27	59	61	57	72
50	38	83	26	21	78	84	64	70	71	86	19	68	29	24	23	28	74	75
39	42	55	82	45	44	46	33	10	41	88	79	12	34	8	54	81	73	48
40	25	7	15	47	35	31	6	14	30	4	87	5	20	32	16	65	9	3
17	13	63	67	22	66	1	43	2	11	49	13							

INCREASING VALUES OF  $\Delta_{e_1}$

34	27	36	76	56	53	58	52	37	33	77	62	60	59	35	38	22	51	55
67	50	61	57	80	86	64	83	78	26	69	85	72	74	70	73	68	75	24
42	71	29	23	39	21	84	40	12	81	46	28	19	79	25	41	32	2	8
10	1	45	14	20	49	43	65	44	88	48	16	47	15	7	4	31	30	6
66	82	11	3	17	18	63	13	5	54	87	9							

INCREASING VALUES OF  $\Delta_{e_2}$

75	76	68	74	72	70	55	69	58	27	34	77	36	51	37	83	35	80	62
52	56	39	53	50	38	59	24	61	57	78	60	26	21	41	23	42	71	85
86	12	84	30	28	33	81	29	19	73	46	45	47	79	25	31	64	43	48
10	40	8	66	15	13	88	44	4	49	20	6	65	87	11	3	17	18	63
16	54	82	9	7	22	5	67	1	32	2	14							

INCREASING VALUES OF  $\Delta_e$

34	27	36	76	56	53	58	52	37	77	62	60	59	35	38	51	55	50	61
57	33	80	86	83	78	26	69	72	74	85	70	68	73	75	24	42	71	29
23	39	21	84	64	12	81	46	28	19	79	40	25	41	10	8	45	43	49
20	44	88	48	65	47	15	16	4	22	31	7	67	30	6	66	82	11	1
3	17	18	63	32	13	2	5	14	54	87	9							

TABLE V

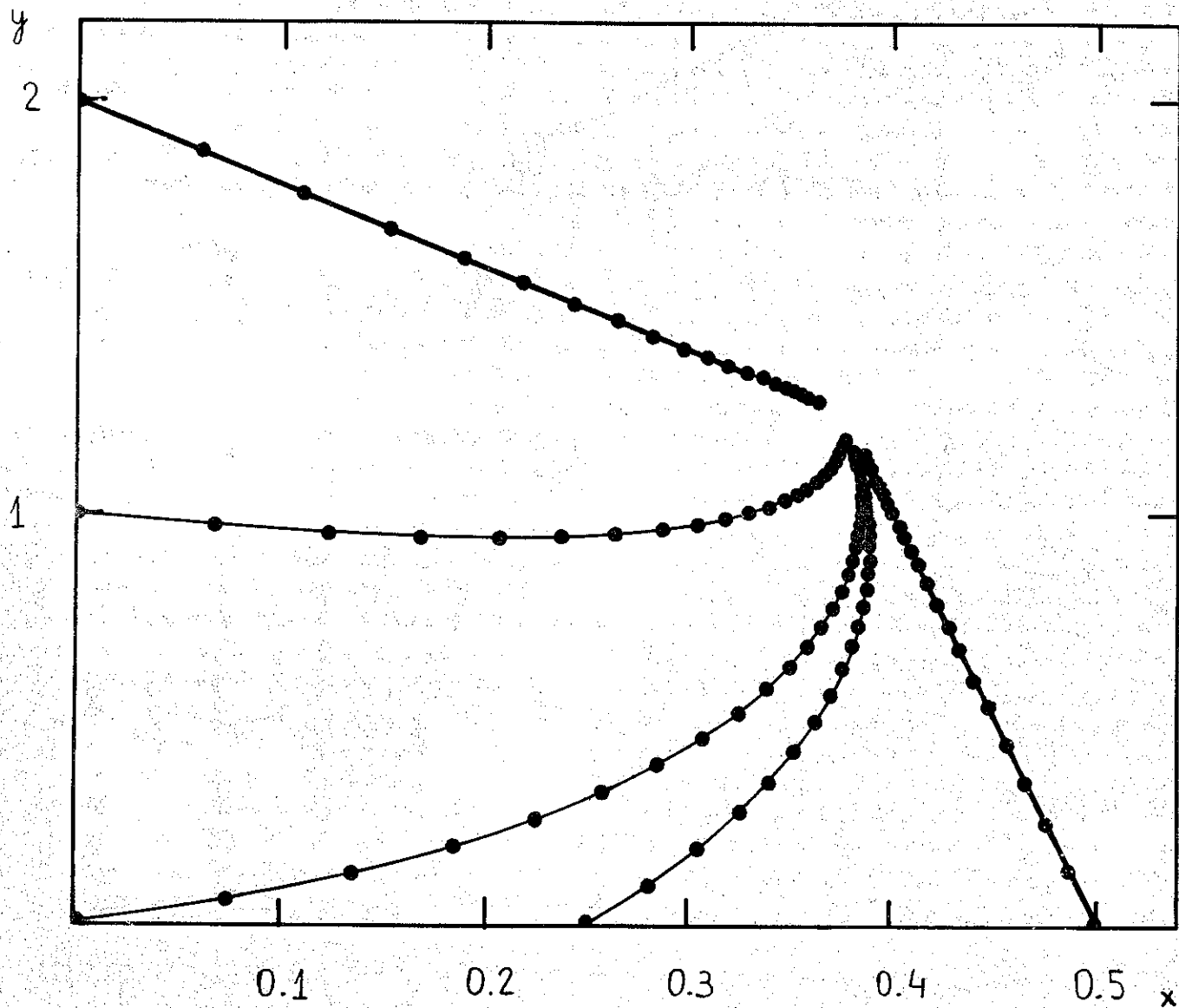


FIGURE 1



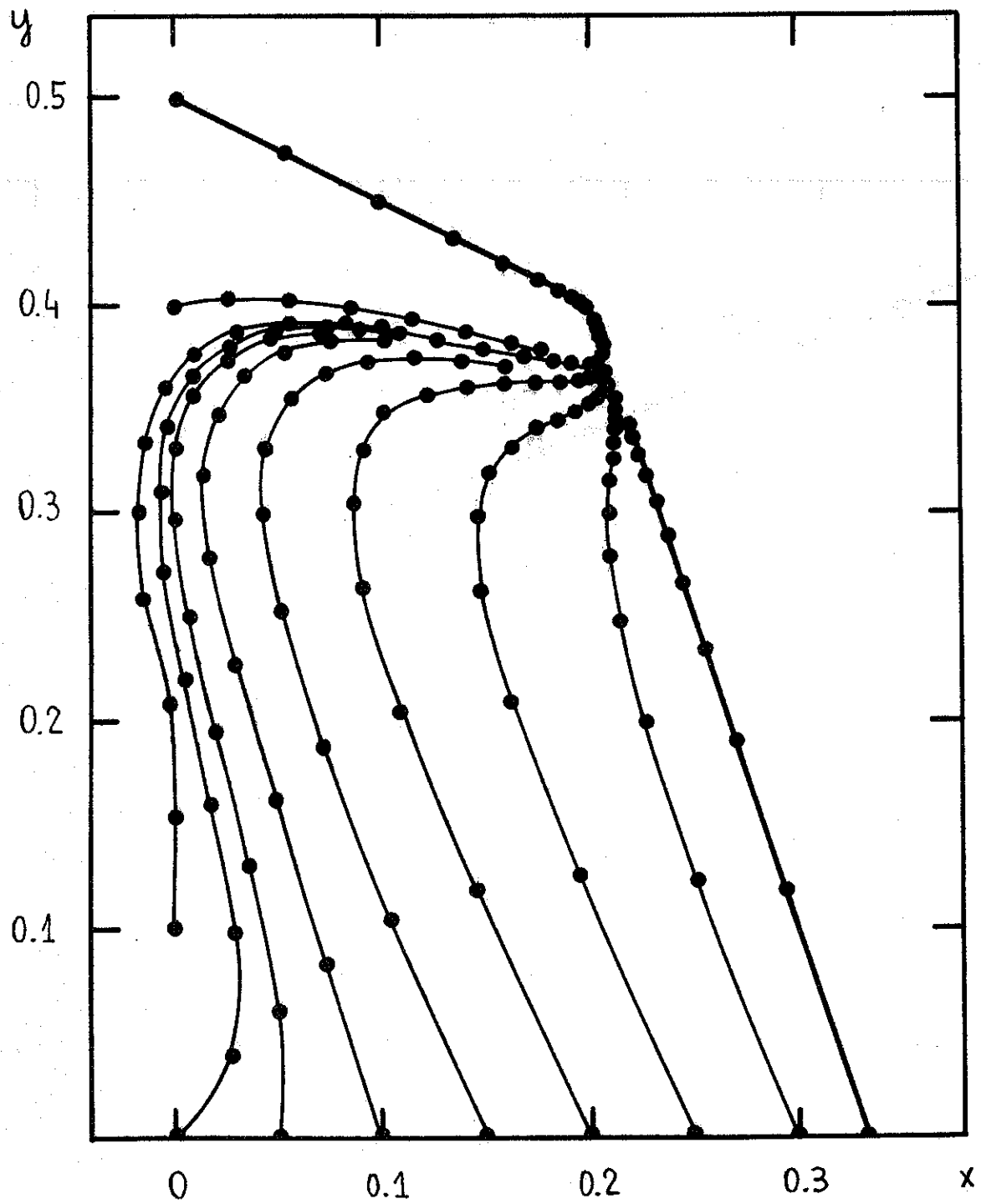


FIGURE 2

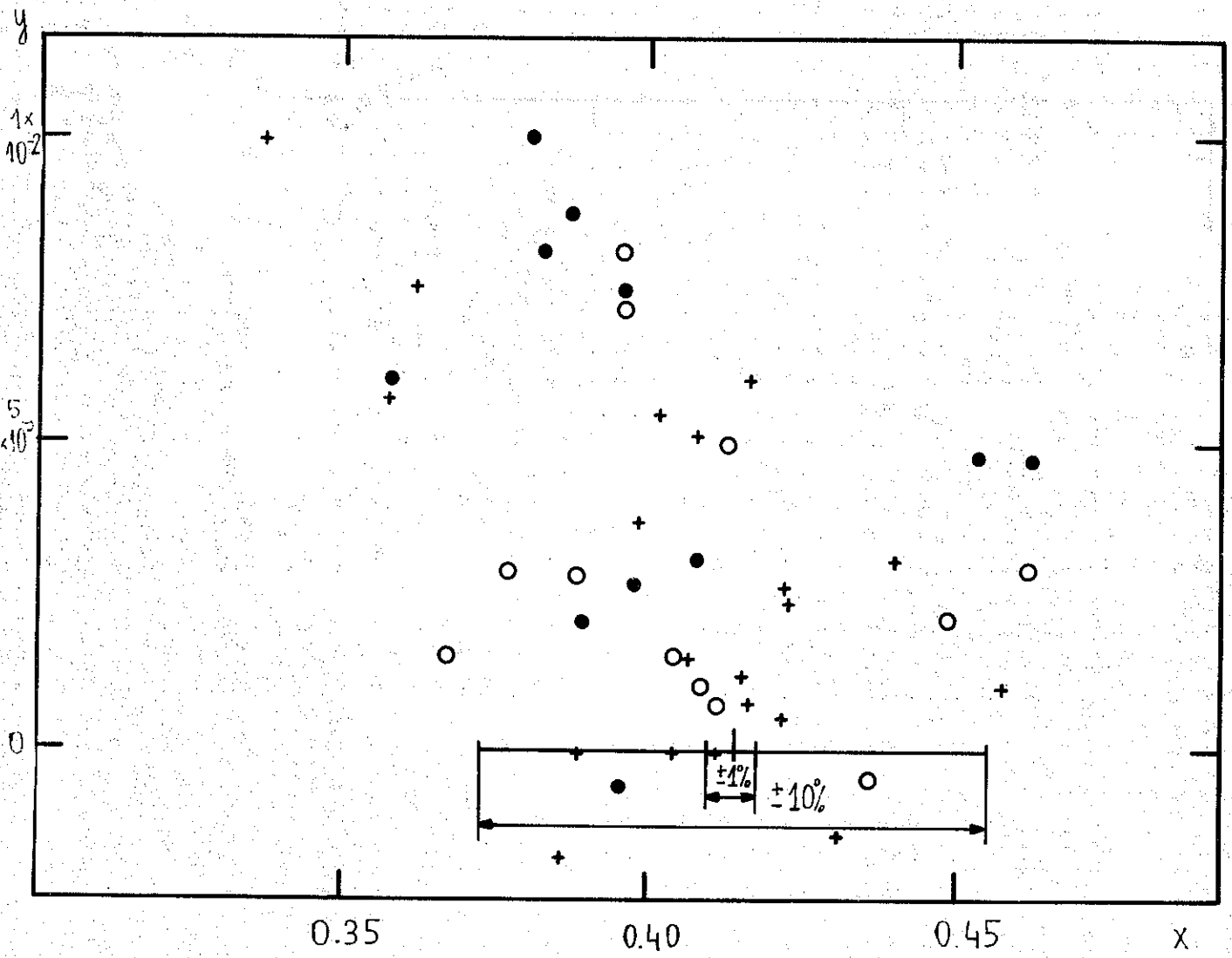


FIGURE 3

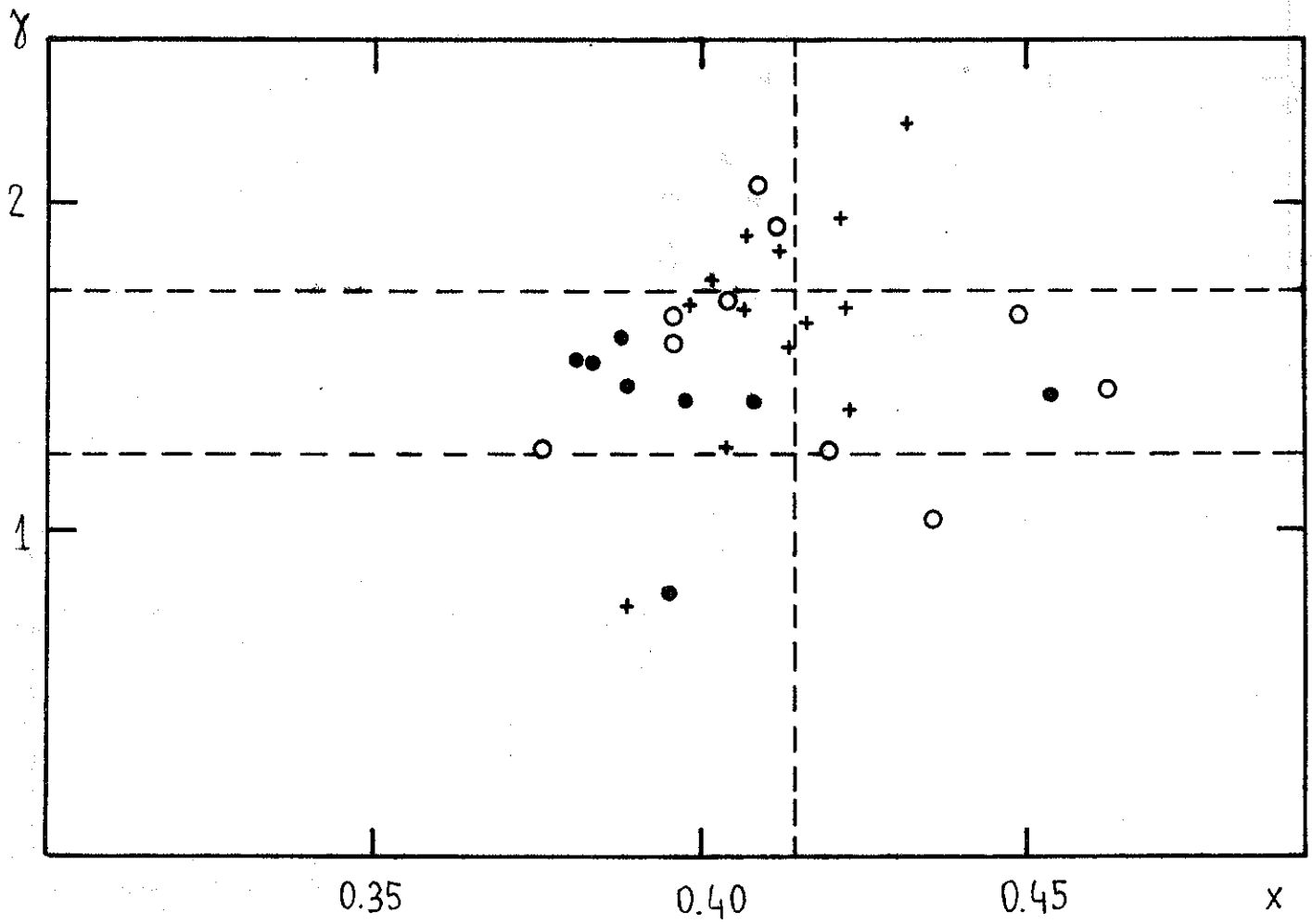


FIGURE 4

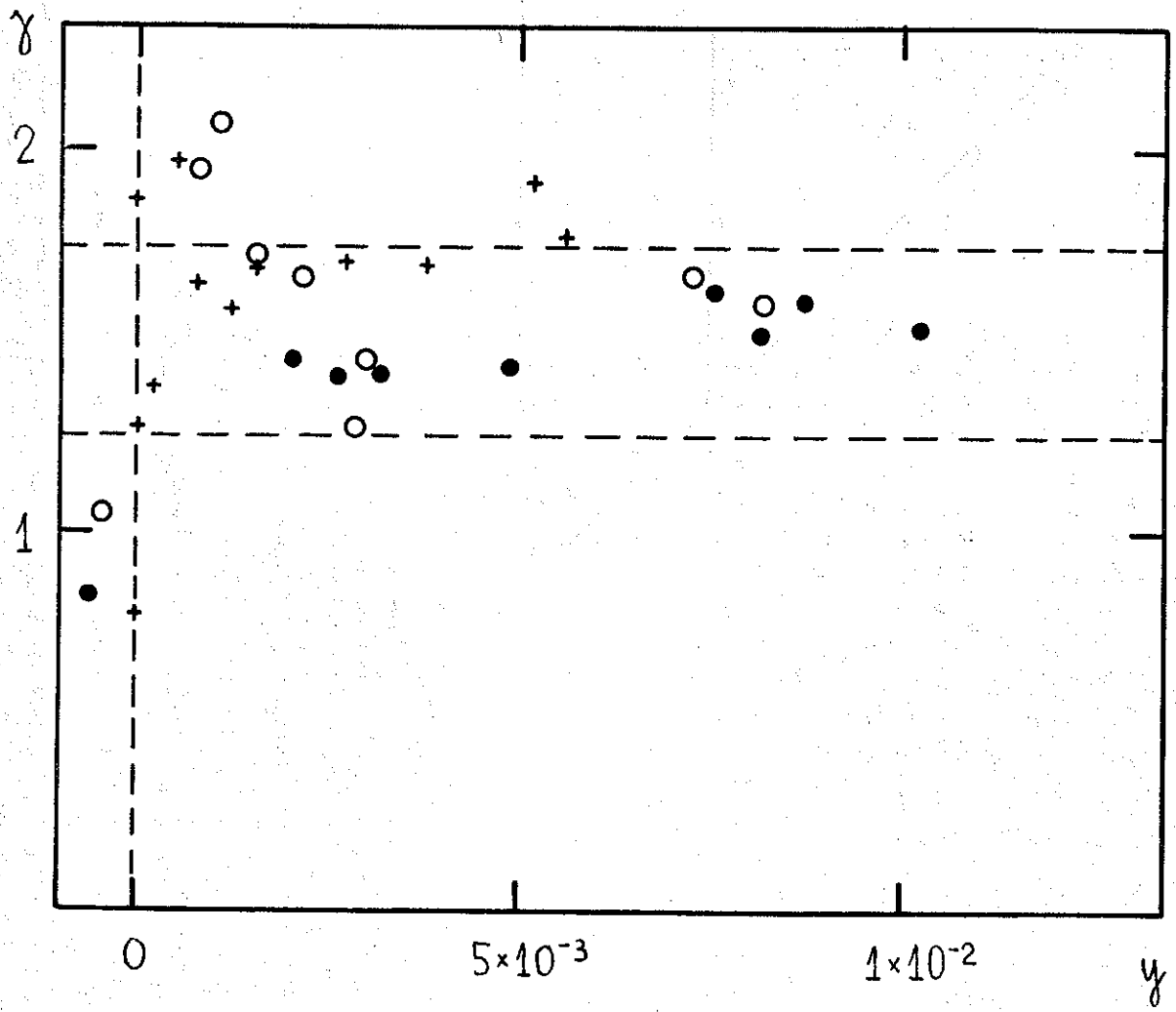


FIGURE 5

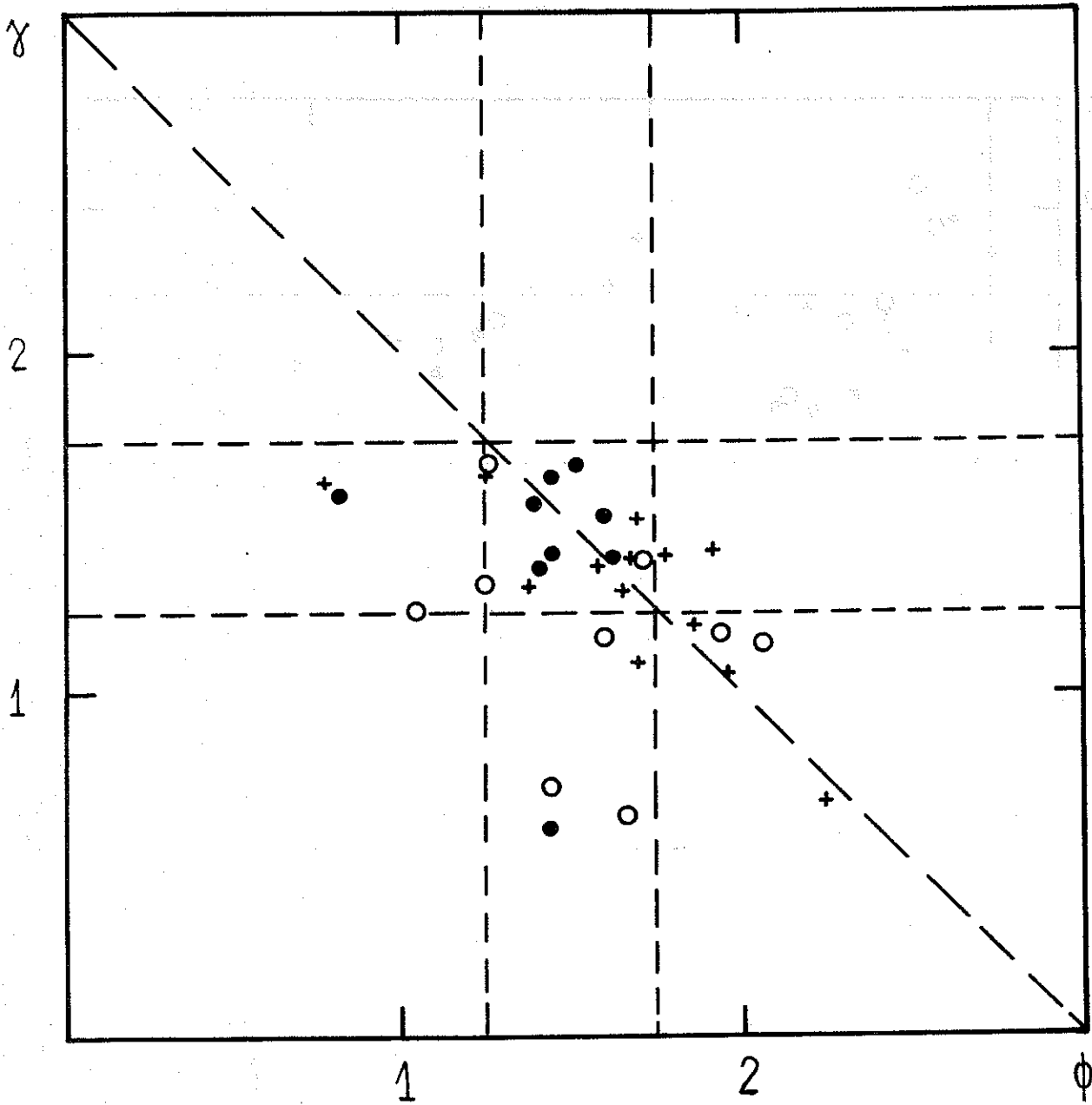


FIGURE 6

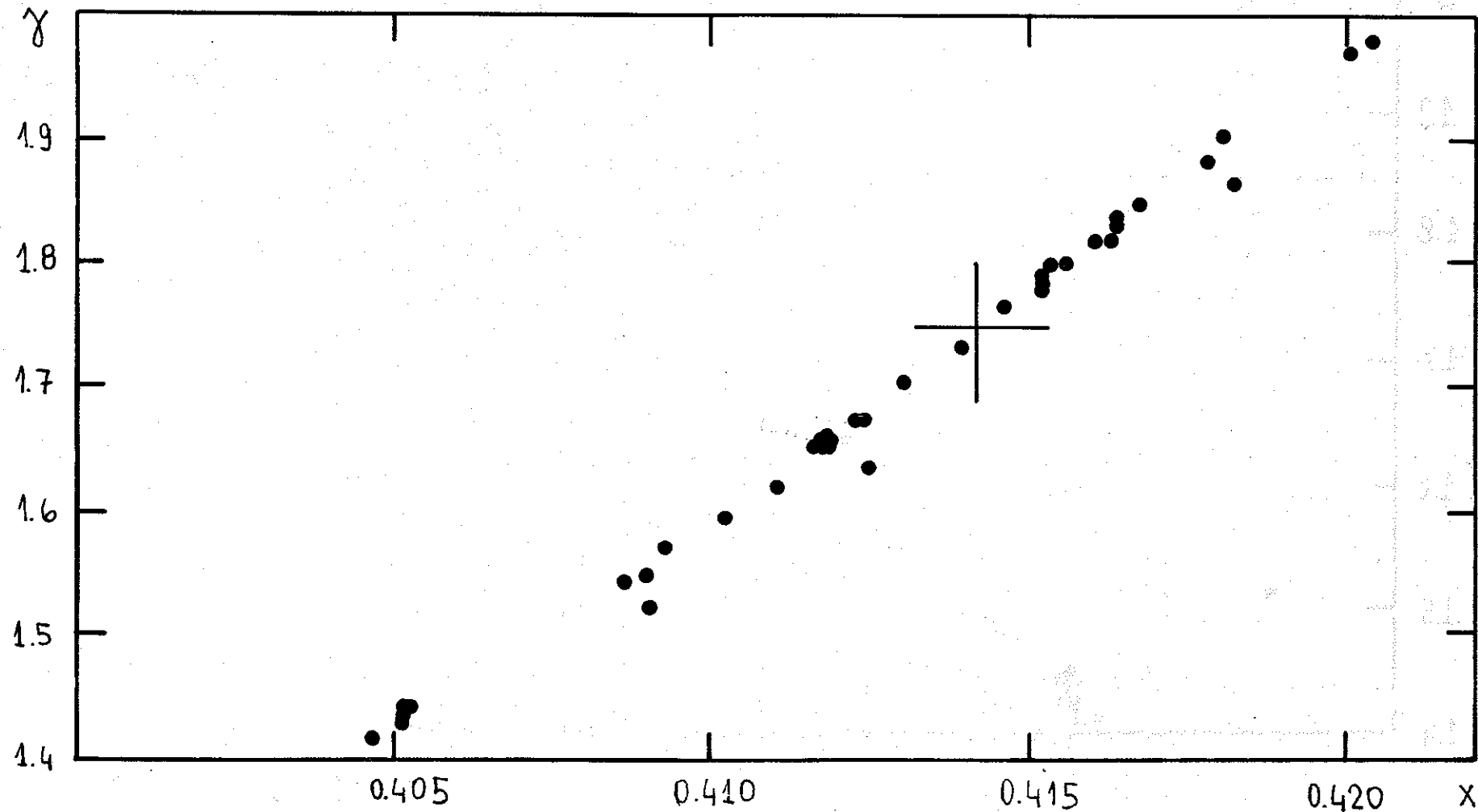


FIGURE 7

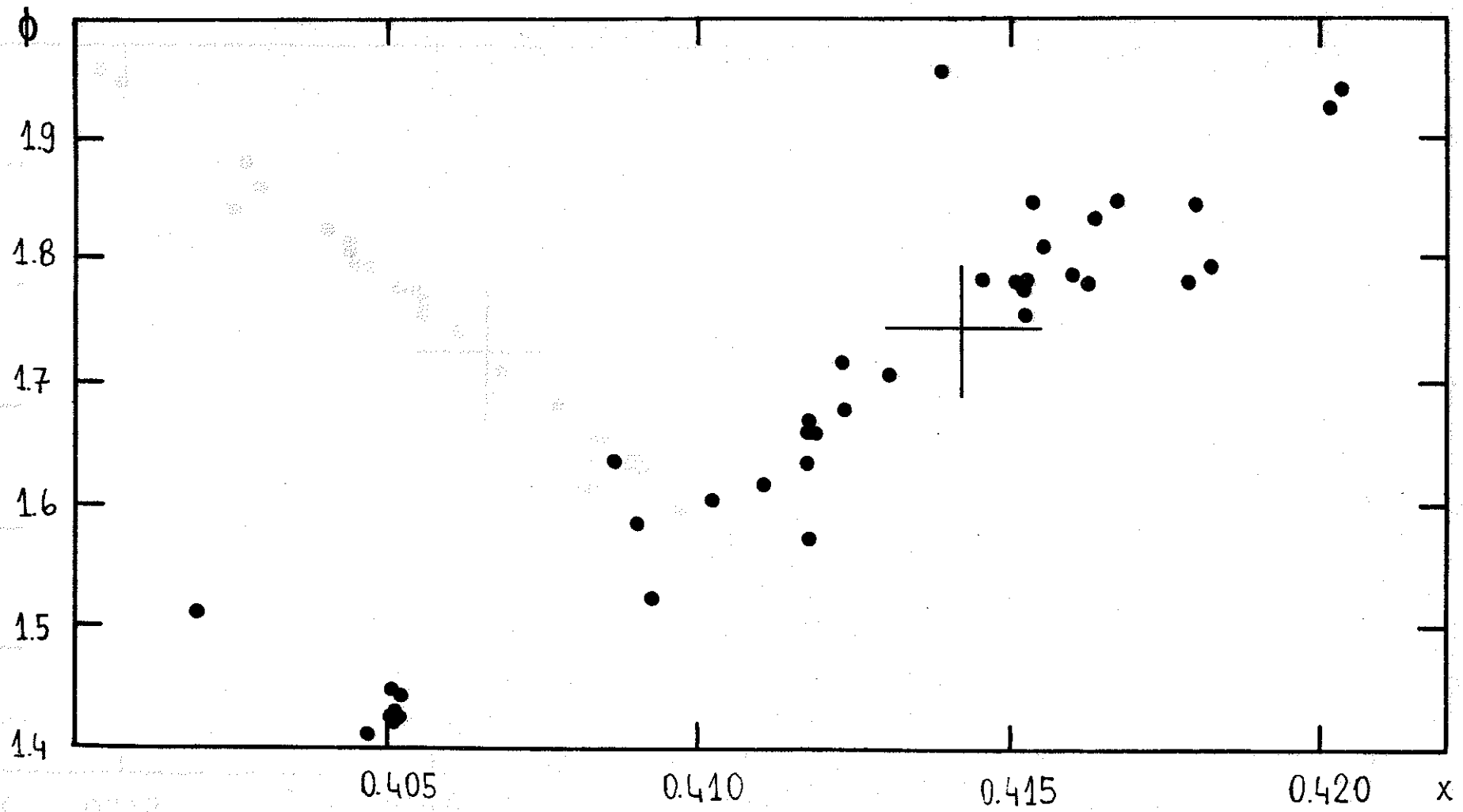


FIGURE 8

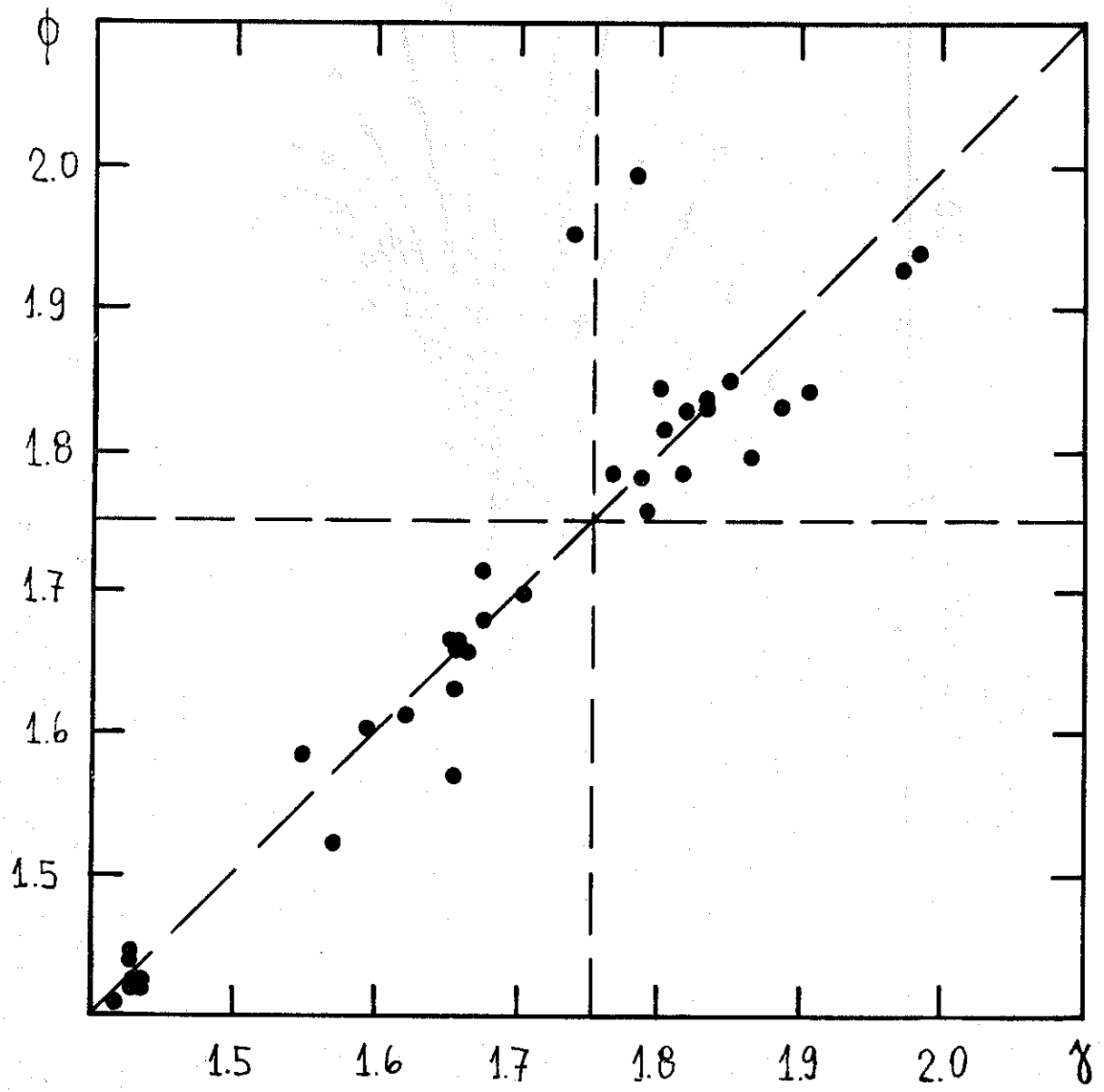


FIGURE 9



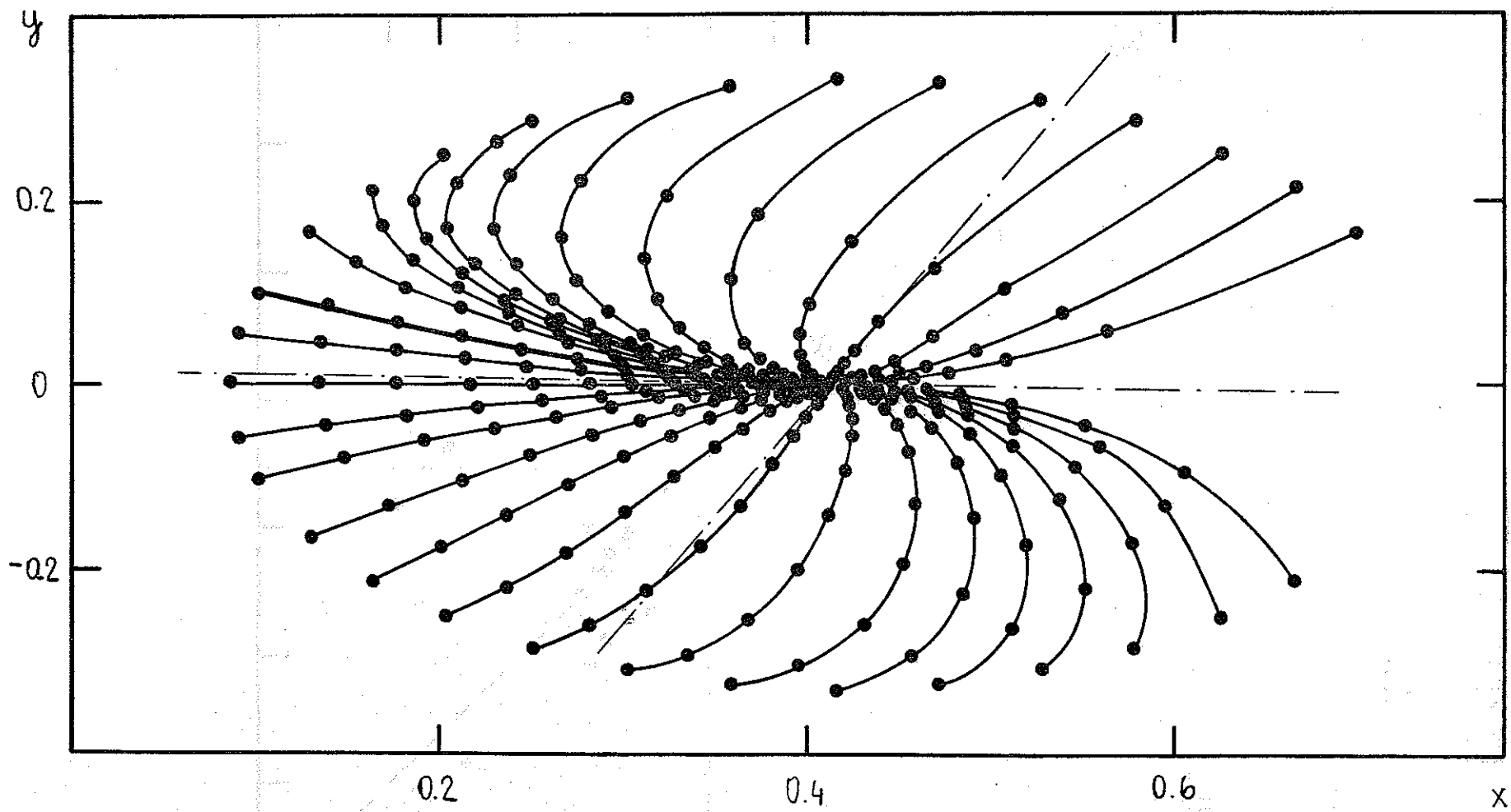


FIGURE 10

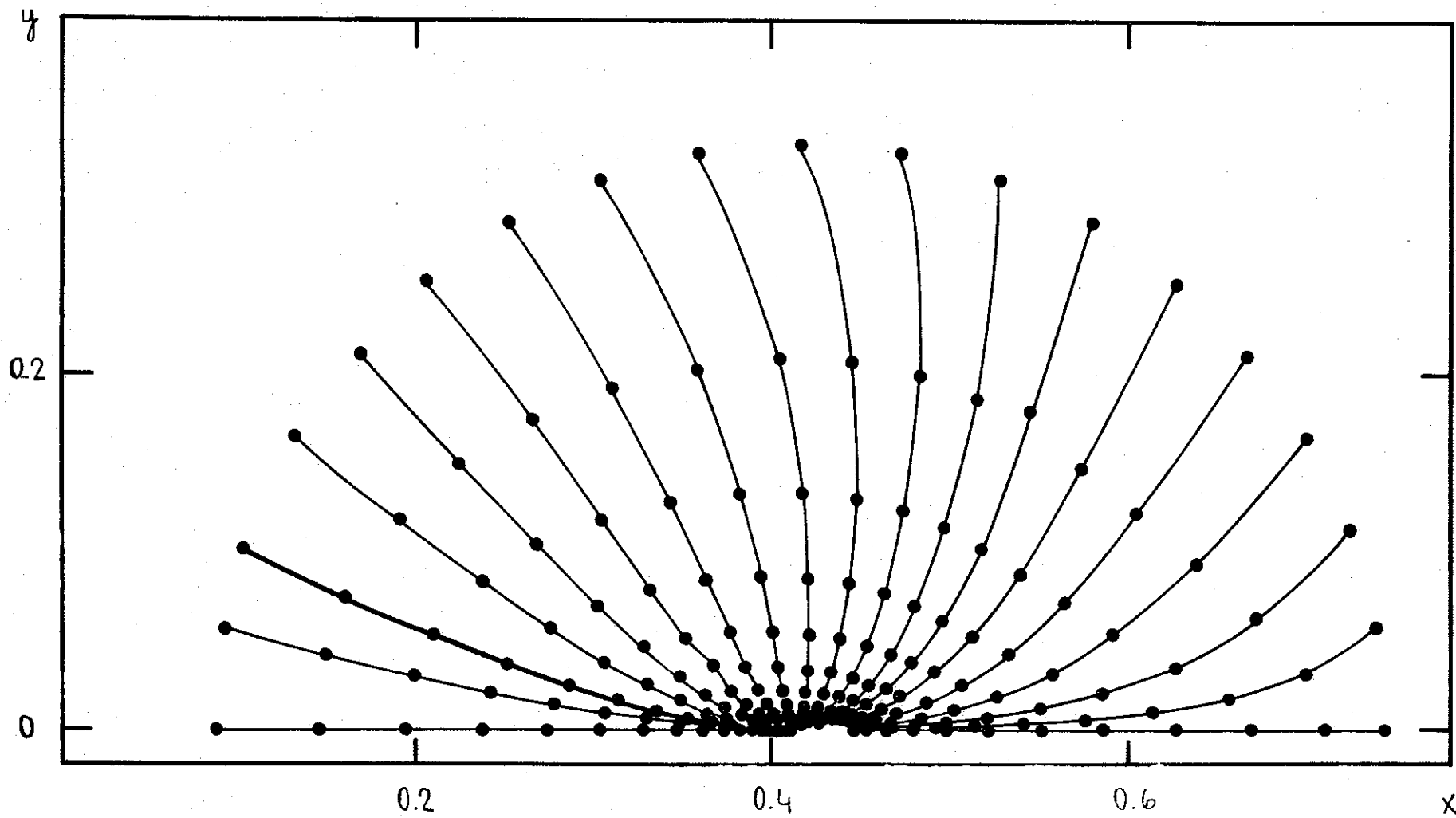


FIGURE 11